Systems and Control
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Introduction to computer control systems Master program in embedded systems, period 2, 2011

Problem solving session VI (Ex6) - Solutions

- 1. System pulse-transfer operator: $H(q) = \frac{k}{q^2 + 0.4q + k} \Rightarrow$ the system transfer function is given by $G(s) = \frac{k}{s^2 + 0.4s + k}$. The roots of the polynomial $s^2 + 0.4s + k$ must lay inside the unit circle for the system to be stable. The system is hence stable if 0 < k < 0.04. Note that k must be greater than zero for the feedback to be negative.
- $2. \quad \text{(a)} \ \ x_0 = \begin{bmatrix} -3 \\ -2 \end{bmatrix}$
 - (b) $\Delta x(k+1) = \begin{bmatrix} 1 & 0.2 \\ 0.5 & 0 \end{bmatrix} \Delta x(k)$
 - (c) $eig(A) = \{1.0916; -0.0916\}$. Since there is an eigenvalue λ_i such that $|\lambda_i| > 1$, the system is unstable.
- 3. (Based on Exercise 3.22 from [1])

NOTE: The (a) part of this question was changed from the one in the list of exercises. Here follows its correct version:

A dynamic system is given by a scalar differential equation with an algebraic expression given by

$$\frac{d}{dt}\xi = -\xi + u\eta^3$$

$$0 = -\eta + u^2 e^{\eta}$$

(a) A control system should be designed to keep the system at a given stationary point ξ_0 . Determine the full operating point (ξ_0, u_0, η_0) when $\eta_0 = 1.1843$ and $u_0 > 0$.

The second equation gives $0 = -\eta_0 + u_0^2 e^{\eta_0} \Leftrightarrow u_0 = \pm 0.6020$. Choose the positive solution for u_0 .

At the equilibrium point $\dot{\xi} = 0 \Leftrightarrow -\xi_0 + u_0 \eta_0^3 = 0 \Leftrightarrow \xi_0 = 1$

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(b) The system input is u and its output is $y = \eta \xi$. Determine a linear state model, valid near the operating point determined in (a). The second equation $0 = -\eta + u^2 e^{\eta}$ gives $\eta = u^2 e^{\eta}$. Replacing η in the first equation, it follows

$$\frac{d\xi}{dt} = -\xi + u^7 e^{3\eta}$$

The linearization of the nonlinear term $f(u, \eta) = u^7 e^{3\eta}$ around the stationary point (ξ_0, u_0, η_0) stands as

$$f(u,\eta) \approx f(u_0,\eta_0) + \frac{\partial f}{\partial u}|_{(u_0,\eta_0)}(u-u_0) + \frac{\partial f}{\partial \eta}|_{(u_0,\eta_0)}(\eta-\eta_0)$$

$$u^7 e^{3\eta} \approx u_0^7 e^{3\eta_0} + 7u_0^6 e^{3\eta_0}(u-u_0) + 3u_0^7 e^{3\eta_0}(\eta-\eta_0)$$

$$\frac{d\xi}{dt} + \xi \approx \xi_0 + 7u_0^6 e^{3\eta_0}(u-u_0) + 3u_0^7 e^{3\eta_0}(\eta-\eta_0)$$

$$\frac{d\xi}{dt} \approx -(\xi-\xi_0) + 7u_0^6 e^{3\eta_0}(u-u_0) + 3u_0^7 e^{3\eta_0}(\eta-\eta_0)$$

By defining $E = \xi - \xi_0$, $U = u - u_0$ and $N = \eta - \eta_0$, and substituting u_0 and η_0 by its values, it follows that

$$\frac{dE}{dt} = -E + 11.6288U + 3N$$

In order to have a linear relation between η and u, $0 = -\eta + u^2 e^{\eta}$ has to be linearized. By using Taylor series expansion around the equilibrium point,

$$\eta \approx u_0 e^{\eta_0} + 2u_0 e^{\eta_0} (u - u_0) + u_0^2 e^{\eta_0} (\eta - \eta_0)
\eta - \eta_0 \approx 2u_0 e^{\eta_0} U + u_0^2 e^{\eta_0} N
N \approx 2u_0 e^{\eta_0} U + u_0^2 e^{\eta_0} N$$

Substituting u_0 and η_0 by its values, it follows that N = -21.3511U. The linearized differential equation is then given by

$$\frac{dE}{dt} = -E - 52.4244U$$

The linearized output is given by

$$y - y_0 \approx \xi_0(\eta - \eta_0) + \eta_0(\xi - \xi_0)$$

 $Y = N + 1.1843E$
 $Y = -21.3511U + 1.1843E$

$$\dot{E} = [-1]E + [-52.4244]U$$
 $Y = [1.1843]E + [-21.3511]U$

- (c) How is the stability of the stationary operating point (ξ_0) ? The linearized system has a pole in -1 so it is stable around the stationary point (ξ_0) .
- 4. (a) SS1: $\overline{c_A} = 0$, $\overline{c_B} = 0$. SS2: $\overline{c_A} = 1/\beta$, $\overline{c_B} = 1/\alpha$. M1:

$$\dot{\Delta c} = \begin{bmatrix} -1 & 0 \\ 0 & -1 \end{bmatrix} \Delta c$$

$$\Delta c_M = \begin{bmatrix} 0.5 & 0.5 \end{bmatrix} \Delta c$$

M2:

$$\dot{\Delta c} = \begin{bmatrix} 0 & \alpha/\beta \\ \beta/\alpha & 0 \end{bmatrix} \Delta c$$

$$\Delta c_M = \begin{bmatrix} 0.5 & 0.5 \end{bmatrix} \Delta c$$

(b) M1 is assymptotically stable and M2 is unstable regardless the values of the process parameters α and β .

References

[1] Mikael Johansson and Torsten Söderström. Exercises Control Theory. Uppsala University and Royal Institute of Technology, 2010.